

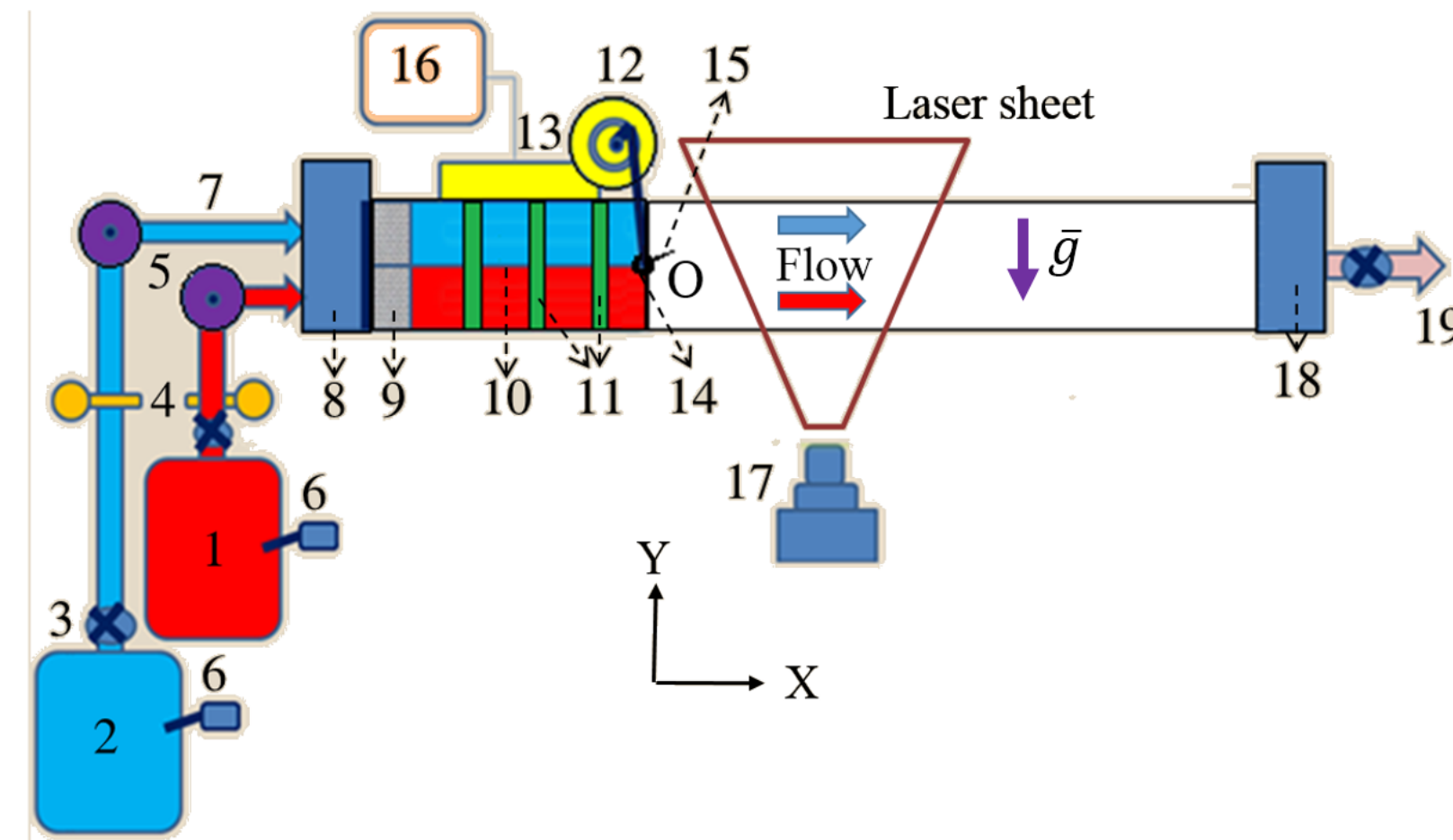
INTRODUCTION

- **Rayleigh-Taylor (RT)** instability occurs when density and pressure gradients are misaligned, i.e. $\nabla P \cdot \nabla \rho < 0$. The baroclinic torque $-\nabla \times (\frac{\nabla P}{\rho})$ is the source of initial vorticity
- In the current study using the Water Channel facility, an initial unstable stratification of cold and hot water streams are acted upon by gravity
- A servo controlled flapper mechanism provides precise initial perturbations at interface of the cold and hot water streams
- Stages of RT evolution with time: Linear \rightarrow Non-linear (**mode coupling**) \rightarrow Turbulent

Motivation

- RTI is observed in many natural phenomena such as clouds, salt-water domes, astrophysical events (e.g. nebulae)
- RTI is also witnessed in several applications such as in the ICF (Inertial Confinement Fusion) and spray ignition in engines etc.

EXPERIMENTAL SETUP



Flow parameters

- $U = 4.5$ cm/s
- $T_{hot} - T_{cold} \approx 5.0^\circ\text{C}$
- $A_t = 1.2 \times 10^{-3}$

Diagnostics

- High resolution imaging
 - Line of Sight (LOS) imaging
 - Thermocouple measurement
 - 1kHz temporal resolution
 - Density field extracted
 - Planar Laser Imaging of Fluorescence (PLIF)
 - 15Hz temporal resolution
 - 2.0MP spatial resolution
 - Concentration (passive scalar) field extracted
 - Particle Image Velocimetry (PIV)
 - 30Hz temporal resolution
 - 1.4MP spatial resolution

- 1. Hot water tank
- 2. Cold water tank
- 3. Valve
- 4. Flow meter
- 5. Pump
- 6. Thermostat
- 7. Piping
- 8. Inlet plenum
- 9. Flow straighteners
- 10. Splitter plate
- 11. Wire mesh
- 12. Servo motor
- 13. Servo controller
- 14. Connecting bars
- 15. Flapper
- 16. Computer
- 17. Camera
- 18. Exit plenum
- 19. Water outlet
- O: Origin

Figure 1: Schematic of the Water Channel setup

PLIF EXPERIMENTAL PARAMETERS

Initial conditions

- Initial condition
- $\frac{a_i}{\lambda_i} = 0.1$
- $\lambda_i = \sum a_i \sin(\omega_i t + \beta_{i-1})$
- $\omega_i = \frac{2\pi U}{\lambda_i}$

Table 1: List of experiments

IC mode type	Remarks	Case #	Wavelength			Phase angle		A_t ($\times 10^{-3}$)
			λ_1 (cm)	λ_2 (cm)	λ_3 (cm)	β_1 (°)	β_2 (°)	
Single	Increasing λ	1	0	-	-	-	-	1.00
		2	2	-	-	-	-	1.00
		3	4	-	-	-	-	1.03
		4	6	-	-	-	-	1.02
		5	8	-	-	-	-	1.06
Binary	Increasing β	6	8	2	-	0	-	1.07
		7	8	2	-	30	-	1.11
		8	8	2	-	45	-	1.11
		9	8	2	-	60	-	1.13
		10	8	2	-	90	-	1.12
		11	8	2	-	120	-	1.88
Binary	Increasing λ_2	12	8	4	-	45	-	1.00
		13	8	6	-	45	-	1.06
		14	8	4	2	45	90	1.10
Multi	Inc. # of modes	14	8	4	2	45	90	1.10
		15	8	6	4	45	-	1.06
		16	8	6	5	45	-	1.11
		17	8	7	6	45	-	1.13
		18						2.00

Analysis details

- Background intensity and laser plane divergence corrected. Linear attenuation of light with y at low dye concentration
- Ensemble average of 800 images used to calculate mixing width. Equivalent wavelength, λ_{eq} based on initial height

FLOW VISUALIZATION

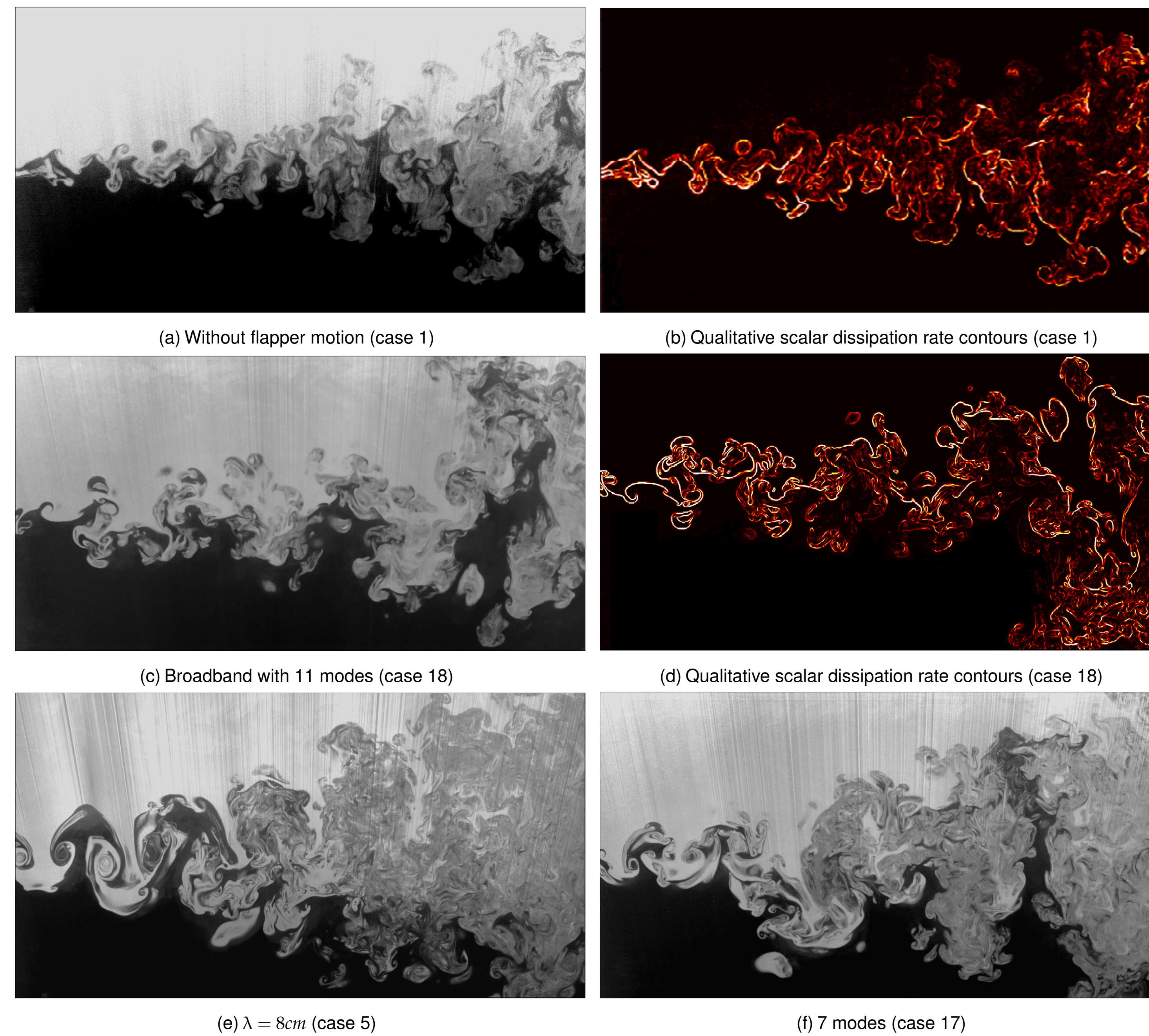


Figure 2: Flow visualization for select cases

EFFECT OF WAKE ON A CONVECTIVE RT SETUP

- The wake interacts with RT evolution. PIV measurement indicates that the wake is highly symmetric about the splitter plate
- The peak wavenumbers in v spectrum (fig. 3(a)) correspond largely to the splitter plate thickness and spacing between the wire meshes
- The molecular mixing parameter, θ , obtained from PLIF images indicate that the effect of the wake in diffusion mixing is very small compared to that of baroclinic vorticity
- χ^* plotted along $y \approx 0$ (fig. 3(c)). Here $t = \frac{x}{U}$ using Taylor's hypothesis

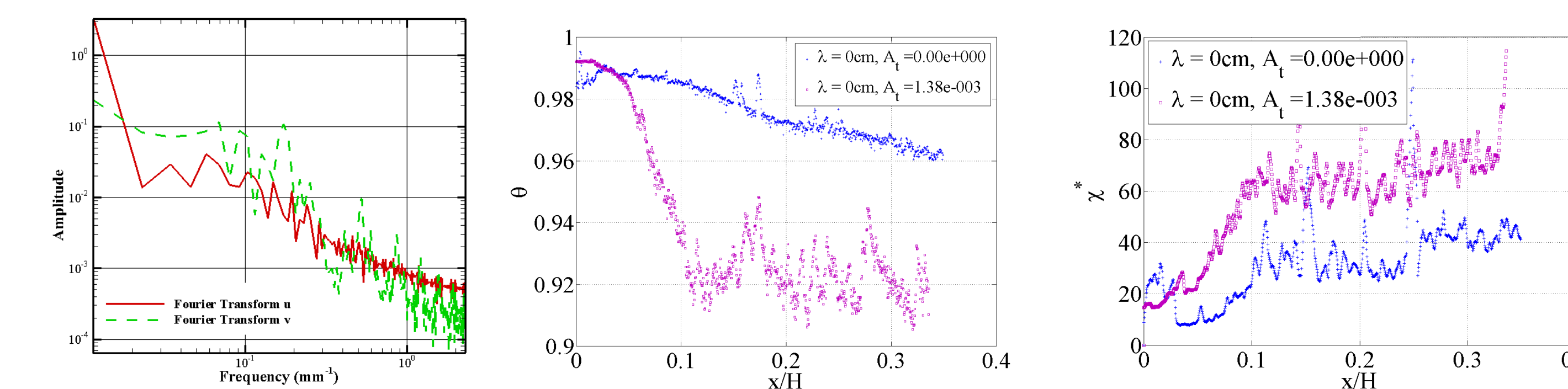


Figure 3: Wake effect on RT mixing

ACKNOWLEDGEMENT

- Thanks to the support of DOE-NNSA SSAA program grant # DE-NA-0001786

NOMENCLATURE & DEFINITIONS

- P Pressure
- ρ Density
- g Acceleration due to gravity
- U Mean convective velocity
- T Temperature
- h Total mixing width, $h = h_{(f_c=0.95)} - h_{(f_c=0.05)}$
- f Mole fraction of fluid
- θ Molecular mixing parameter, $\theta = 1 - \frac{B_0}{B_2}$
- $B_0 = \lim_{T \rightarrow \infty} \frac{1}{T} \int \rho'^2 dt / (\rho_c - \rho_h)^2$, $B_2 = f_c f_h$
- B_0 Density fluctuation self-correlation for miscible fluids
- B_2 Density fluctuation self-correlation for distinct fluids
- t Time, $t^* = \frac{t}{\tau}$, with time scale, $\tau = \sqrt{\frac{\lambda_{eq}}{A_t g}}$
- T Total time of observation
- χ Instantaneous scalar dissipation, $\chi^* = \int_{-H/2}^{H/2} \frac{|\nabla \cdot \langle f_c(x,y) \rangle|^2 dy}{Sc H}$
- Sc Schmidt number
- H Total channel height
- λ Wavelength of initial condition
- y Displacement of initial condition
- a Amplitude of initial condition
- ω Angular frequency
- β Phase angle of initial condition
- Pr Prandtl number
- u Streamwise velocity
- v Spanwise velocity
- (x, y, z) Coordinates (refer fig. 1)
- Subscripts**
- ' Fluctuation
- * Non-dimensionalized
- Subscripts**
- c Cold
- h Hot
- eq Equivalent
- $\langle \rangle$ Time mean

RESULTS & DISCUSSION

RT Mixing study

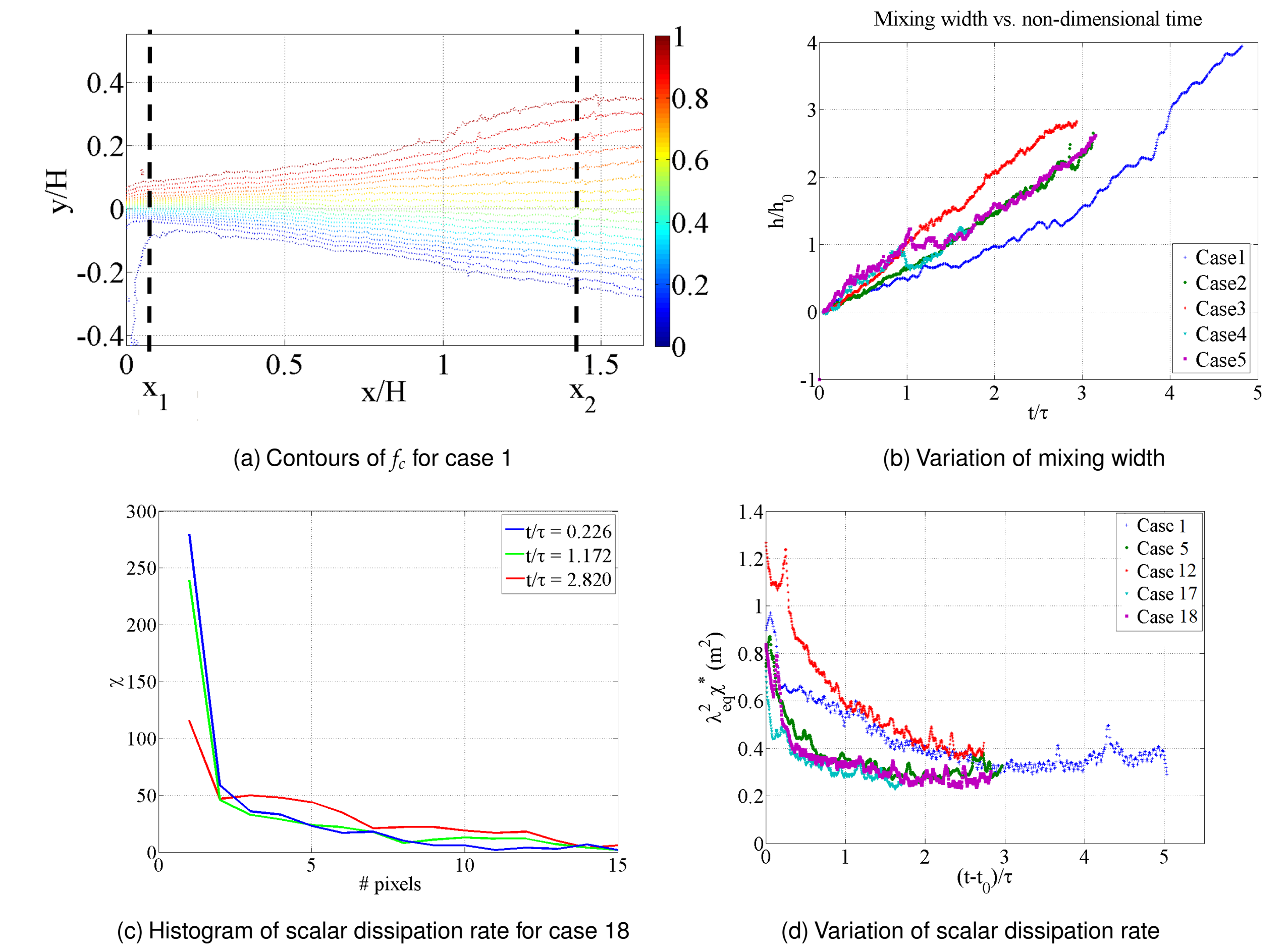


Figure 4: Variation of integral mixing parameters

CONCLUSION & FUTURE WORK

- In the mode coupling regime, the growth rates are comparable with each other for different cases (fig. 4(b)). However, saturation has not been attained for many cases
- The fastest growth rate is of the broadband case while the slowest corresponds to the no flapper motion case.
- Scalar dissipation rate scales as λ_{eq}^{-2} and flattens out at late-times, showing independence of fine-scale mixing (fig. 4(d))
- Simultaneous PLIF + PIV data of these cases will help study of flow characteristics such as anisotropy and saturation, and validation of computational RT codes